## Novel Approaches for Measuring Frequency Converted Group Delay





**ABSTRACT** Frequency Spectrum is a limited resource. There is continual pressure to utilize this resource more efficiently. The end result is that transmitters and receivers must accommodate higher order digital modulation techniques, such as CDMA and OFDMA, to accommodate higher data rates in limited bandwidths. This leads to more effective sharing of the frequency spectrum, and also higher data rates and quality of service options for the end customer.

This places stringent demands on the design of the transmitter and receiver. In particular, linear distortion performance such as frequency amplitude response and group delay variation become more important. These parameters have a direct impact on the error vector magnitude (EVM) performance of the system, which ultimately determines the amount of data or information that can be transmitted across the channel.

In this presentation we will review the concepts of group delay, frequency dispersion, and deviation from linear phase. We will show the EVM performance of a channel with different amounts of group delay variation to directly see the impact of group delay variation. We will also review a variety of techniques for making group delay measurements, including envelope delay, phase measurement on a multi-carrier signal, S parameter techniques, reference-mixer techniques, a new VNA technique without LO access, and finally a vector corrected S parameter measurement on a mixer or receiver with LO access. The second part of this presentation will explore existing NF measurement techniques, and introduce a new VNA-based technique.

Each measurement has its place, trading off parameters such as complexity, accuracy, measurement speed, and cost. By reviewing the available techniques, the engineer will be better prepared to select the best approach for a particular application.

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# Outline (slide 1 of 2)

#### What is Linear Distortion?

- Frequency Response
- Phase ripple
  - Deviation From Linear Phase
  - Group Delay
  - Dispersion
- Impact on EVM





# Outline (slide 2 of 2)

#### Methods of Measuring Group Delay and Phase Response

- Time-based
  - Gaussian Pulse
  - FM modulation & Envelope delay
- Multi-Carrier signal and delta phase
- Network Analyzer, 2 port S-parameters
- Network Analyzer plus *frequency translation*, now what?
  - Relative measurements with reference mixer

- LO recovery technique for embedded LO
- 2 tone Network Analyzer approach for embedded LO
- Full error correction via adaptor removal technique with a mixer
- Full error correction via unknown through technique with a mixer





## Interesting Questions...

- What is group delay?
- Can we have a negative group delay?
- Does group delay = signal delay through a device?
- Does a CW signal "experience" group delay?
- If I know the group delay of a device, do I know it's insertion phase?
- What is phase delay?
- Is group delay a "linear" or "non-linear" distortion?
- Can group delay be compensated? Perfectly?

Page 5

- Is group delay required to measure deviation from linear phase?
- What is the "correct" way to measure deviation from linear phase?



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#### Sinusoids

#### Sinusoids are defined by three parameters

- Frequency
- Amplitude
- Phase



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#### Sinusoids – parameters we can modify

Amplitude

Frequency or Phase 

Page 7



time



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#### **Modulation Methods**

- We vary the amplitude and phase to transmit information
  - Analog modulation: AM, FM, PM
  - *Digital modulation:* FSK, BPSK, QPSK, 16 QAM, and more...

- We use different techniques to share the channel
  - FDMA, TDMA, CDMA, OFDMA, MIMO and others....

Page 8



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## Sinusoids and Distortion

- Amplitude response variation (or ripple) vs. frequency results in linear distortion of the input signal's amplitude.
- Phase response variation (or ripple) vs. frequency results in linear distortion of the input signal's phase.
- Linear Distortion is distortion of the signal that is *independent* of the signal's envelope level.

Page 9



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 This is in contrast to NON-Linear Distortion, which is related to the signal's envelope level. For example, compression, AM-PM distortion, 2<sup>nd</sup> order and 3<sup>rd</sup> order non-linearities are examples of NON-Linear Distortion.



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# **Amplitude Distortion**

- Easy to comprehend
- Some frequencies are transmitted well, others are attenuated.
  - Example
    - Listen to a recording of a band or a CD.
      - · Missing the highs and lows
      - Doesn't sound "live"



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- Playback with an equalizer
  - Restore the correct amplitudes by adjusting gain at different frequencies
  - · Goal is to restore the original amplitude levels
- This is "linear" compensation. It doesn't matter what we play back, the equalizer, once adjusted, can compensate any "sound."
  - As long as it isn't attenuated to the level where the S/N ratio is no longer satisfactory



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#### **Amplitude Distortion**

• Example of Amplitude Compensation:



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# Phase Distortion



- Not as intuitive, needs more study
- So we end up with
  - Deviation from Linear Phase
  - Group Delay
  - Dispersion

Additional terms to → help us explain phase distortion.

- Like amplitude distortion, phase distortion is different amounts of phase shift at different frequencies.
- A phase equalizer would is just as effective as an amplitude equalizer.



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#### What makes this confusing?

- A linear phase response results in a *sloping line*.
- The amount of slope depends on the DUT's insertion delay
- Any slope is ok, as long as it is a "straight" line
- So to measure phase distortion, we need to know how straight the line really is
- So we measure the "deviation" from straight line, or deviation from linear phase in order to measure phase distortion.



- Why does a phase response have a sloping line?
  - Each frequency passed through a transmission line will have a different amount of phase shift due to its wavelength.



Consider this phase response vs. frequency



• Draw a straight line that represents <u>no</u> phase distortion.





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- To measure deviation from linear phase, we first "tilt" the response until it most closely fits a horizontal line.
- Then we consider how much it deviates from this horizontal line at each frequency.



#### Phase Distortion & Group Delay

• Group Delay is defined as:

$$\tau = -\frac{d\phi}{d\omega} (\text{in time})$$

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- Slope of the green "curve fitted" line represents nominal group delay over frequency range.
- The deviation from linear phase is our phase distortion.





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## Phase Distortion and Group Delay

- Group delay is also a measure of how long it takes for a signal's information to propagate through a channel or device under test.
- So there are times when we also care about group delay even when we do not care about phase distortion...
- Example: Gaming on a cell phone...





## Phase Distortion and Dispersion

- Now that we opened the door on derivatives, we can also consider the derivative of group delay with respect to frequency.
- This is a measure of the signal's frequency dispersion.
- Dispersion is another way of describing linear distortion.





#### Real world example: OFDMA and EVM

- Consider an OFDMA signal that is 20 MHz wide, 1201 subcarriers
- With "nearly flat" amplitude and phase response...
  - EVM is ~ -55 dB; a fairly low value.



Rohde & Schwarz EUTRA/LTE Analysis Software Version 2.3 Beta

#### Real world example: OFDMA and EVM

- Introduce "linear" amplitude and phase distortion via a channel filter, which primarily impacts the band edges...
  - Approximately 0.5 dB of amplitude response
  - Approximately 2.5 nS of group delay response
- EVM is now -35 dB at the band edges



# Methods of Measuring Group Delay

- Timing-based methods
  - Gaussian Pulse
  - FM modulation & Envelope delay
- Multi-Carrier signal and delta phase
- Network Analyzer, 2 port S-parameters
- Network Analyzer plus frequency translation, now what?
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## Timing method of measuring group delay

- Use a VSG and a VSA
- Send a "pulse" through the DUT.
- Send a marker to the VSA telling it when to start timing
- Measure the arrival of the pulse relative to the marker
  - Simple subtraction tells us the transit time of the pulse



# Timing method of measuring group delay

- Cautions:
  - This measures the delay through the test equipment and DUT
  - Normalization can be utilized to address this
    - Remove the DUT, measure the starting time delta





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# Timing method of measuring group delay

• Example: Measure internal delay between marker and RF pulse on a Rohde and Schwarz SMU Vector Signal Generator





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#### Results of 21 manual measurements using Tek Scope:

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Page 30



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#### • Now repeat the measurement using a Rohde and Schwarz FSQ.

• Automate it this time, manual measurements take too long.



SMU 10 MHz reference out connected to FSQ 10 MHz reference in.

#### Results of 1001 "automated" measurements, SMU to FSQ



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- This technique allows us to measure group delay with a standard deviation that is < 1 nS.</li>
- Works well for devices that have >> 1 nS of group delay.
- Also works with frequency translating devices...



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#### FM Modulation (envelop delay) Method



#### Measurement Details (envelope delay)

- FSQ can capture the FM modulated carrier within its digital IF.
  - Utilize one of the two A/D convertors
- Simultaneously, the FSQ can capture the low frequency reference path signal, which is the modulating tone for the RF carrier.
  - Utilize the second A/D convertor
- These signals are captured and stored simultaneously with the same capture clock.
- So we can compare the arrival time of the two signals.



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#### **Measurement Setup**



#### **Measurement Setup**

- This is a technique that is similar to the Gaussian Pulse.
- We still have the ability to test frequency converting devices.





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#### Multi-carrier technique

- Up to now we have been "timing" the arrival of the signals as a method of measuring the "group delay" directly.
- An alternate approach exists if we look at the phase shift of multiple carriers across frequency instead of directly at the timing of the signals.



#### Multi-carrier technique

• And we can inject more than two tones. We can use as many as we like to make a very quick wideband measurement.



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#### Multi-carrier technique

- We are measuring phase shifts across frequency instead of "timing"
- We do not really have to measure the phase of the carriers at the input to the DUT. We can normalize the results instead
- Frequency converting devices are still an option
- But notice, no reference path or connection is needed between the input and the output of the DUT. *This is new. Note this, we will use it again...*



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#### **Vector Network Analyzer**

- Traditionally:
  - A Vector Network Analyzer is an ideal instrument for making magnitude and *phase* measurements.
  - It can easily make group delay measurements.
  - It is optimized for speed.
  - Offers full error correction.

This is the instrument we have been looking for...





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#### **Vector Network Analyzer**

- So what is the drawback?
  - Input and output frequency to the DUT have to be the same.
  - Doesn't work with mixers, amplifier harmonics, doublers, prescalers...
- So far every other method we discussed was able to handle frequency translation...
  - But they did not offer full error correction.

Page 45

• Of course we want to combine frequency conversion with full error correction. So let's move in that direction.

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#### Add a reference (mixer) path

- Reference mixer provides a "phase reference" at the IF frequency.
  - As a reference path, it needs to have linear phase & flat group delay response
- Now we can make measurements looking at phase shifts through the DUT
- And we can calculate the group delay "relative" to the reference path.



Page 47



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Calibrate with a "golden" mixer



- Drawbacks of reference mixer approach
  - Normalized measurement, can't achieve full error correction
  - Need access to the LO of the DUT for the reference path
- But, this is perfect for making deviation from linear phase measurements.
  - Easy to setup, especially on a four port network analyzer.
  - Easy to normalize. Wizard available from R&S.





#### • Timing

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#### VNA plus embedded LO: LO recovery

- Without access to the LO, one option is to create an external LO signal, and adjust its frequency until it matches the embedded LO's frequency.
- This can work if the embedded LO is very stable.





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Page 52

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### VNA plus embedded LO: LO recovery

#### Drawbacks of LO recovery

- Normalized measurement, can't achieve full error correction
- LO needs to be very stable.
  - Preferably it will share a 10 MHz reference with the VNA.
- More effort to "find" and adjust to the LO frequency.





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• Without access to the LO, a second option is to use two tones to make the measurement.



• As before, we compare the phase of the two tones before and after the DUT. The shifts tell us the insertion phase of the DUT

$$\Delta \phi = (\phi 1 \text{out} + \phi \text{LO-} \phi 2 \text{out} - \phi \text{LO}) - (\phi 1 \text{in} - \phi 2 \text{in})$$





- Technique is similar to the previously described approach using a signal generator and a spectrum analyzer.
- When adapted to a dual source VNA, however, it is much more compelling as a single box approach, completely automated.



- This approach can tolerate a large amount of LO drift.
- Also works very well with multiple conversion stages in the DUT.

 $\cos((f_2 \bullet t) + \varphi_2 in)$ 

 $\cos((f_1 \bullet t) + \varphi_1 in)$ 

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Page 57

 $\rightarrow$ 



#### Advantages of the two tone approach

- Much more tolerant of a drifting LO
- No need to "find" and estimate LO frequency to a high degree of accuracy
- Simple to setup and start a measurement

Page 58

- There is no "reference" path
- Ability to measure absolute delay by using a calibration mixer



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- Timing
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Page 59

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### VNA plus full error correction

- This approach uses the "adaptor removal" technique of calibration.
- Calibrate port 1 twice, once without the calibration mixer, a second time with it.
  - Requires a "reciprocal" mixer
- This provides the VNA with knowledge about the mixer so it can be "subtracted" from the calibration.
- One reference mixer is utilized to provide the IF with a phase reference.



Setup to characterize the mixer

Page 60

Setup to calibrate the analyzer





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#### The New R&S Solution – Test Setup

- Re-conversion of IF • frequency at Port 2 back to **RF** frequency
- Use of same LO for reconversion and for mixer under test (MUT) (eliminates LO phase and frequency shift)
- Filter to select desired IFband



## VNA plus full error correction

- This approach uses the "unknown through" calibration technique.
- A pair of auxiliary mixers provide the IF receiver with a phase reference.
- Unknown through requires a reciprocal mixer during the "through" calibration.





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### VNA plus full error correction





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Page 64

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#### Review of the methods

#### • Timing

- Gaussian Pulse
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#### ZVA-K9: Mixer Group Delay Measurement without LO Access



### Group Delay – Two Tone Method (Patent Pending)



- Two signals at frequencies f1 and f2 injected into the DUT
- Phase shifts at the output due to the phase response of the DUT

$$\Delta \mathbf{f} = \mathbf{f1} \cdot \mathbf{f2} \quad \Delta \varphi = \varphi 2 - \varphi 1$$
$$\tau = \frac{-1}{360^{\circ}} \cdot \frac{\Delta \varphi}{\Delta f}$$

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Page 67

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### The Measurement (Patent Pending)

- Stimulation with a two carriers f1 and f2 (=f1+ $\Delta$ f)
- Measurement of phase difference of the input signals ( $\phi$ 1in  $\phi$ 2in)
- Phase shift of  $\phi 1 out$  and  $\phi 2 out$  due to the phase response of the DUT
- Measurement of phase difference of the output signals (φ1out - φ2out)

$$>$$
Δ $φ$  = ( $φ$ 1out -  $φ$ 2out) - ( $φ$ 1in -  $φ$ 2in)

Page 68





#### The Measurement of a Converter



- <u>Any</u> LO phase is added to φ1out and φ2out by <u>same amount</u>
- The <u>difference</u> of  $\varphi$ 1out and  $\varphi$ 2out is <u>independent</u> of the LO phase

$$\rightarrow \Delta \phi = (\phi 1 out + \phi LO - \phi 2 out - \phi LO) - (\phi 1 in - \phi 2 in)$$



#### Digital *Dual* Receiver Frontend of ZVA



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## Using 'Wave Quantities





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#### The Measurement

- Measurement of phase difference ( $\varphi$ 1in  $\varphi$ 2in) of both input signals with dual receiver frontend of Port 1
  - Analog down conversion to IF (20 MHz) with LO2 (=LO1-LO) (to measure f1 and f1+df)
  - Digital down conversion to IF (0 Hz) with 2 numeric controlled oscillators (NCO), frequency offset = df
- Measurement of phase difference ( $\varphi$ 2out- $\varphi$ 2out) of both input signals with dual receiver frontend of Port 2




# Accessing 'Wave Quantities for Measurement

More Ratios	
Define Ratio Numerator:	✓ a 1 ✓
Denominator:	💌 a' 1 💌

More Ratios	
- Define Ratio — Numerator:	✓ b 2 ✓
Denominator:	🔽 b' 2 🔽

(φ1in - φ2in)

(φ1out - φ2out)



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Page 73

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### Wave Quantities and Ratios







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Page 74

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Page 75

## ZVA Basic Test Setup: <u>External</u> Power Combiner



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# The ZVT20 Setup (with Internal Combiner)

#### **Close-up View:**

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Page 77

#### The ZVA Setup with Internal Coupler (as Combiner)

Note: This Setup *NOT* recommended for low-freq IF upconverters (70, 140 MHz) due to Coupler Loss



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#### Calibration

- Calibration with known Cal Mixer
- Calibration with ideally assumed Cal Mixer e.g. ZX05-153 (400 ps delay)
- Normalization at RF frequency

Page 78



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#### The User Interface

Define Mixer Delay Measurement without LO Access 🖉 🔀		
Source Lower Tone: Port 1 Upper Tone: Port 3 Config Ext Generators Aperture: 10 MHz	Receiver         DUT Connections         Receiving Port:       Port 2         Driving Port:       Port 1         Meas Bandwidth:       10 kHz         Measurement Bandwidth must be greater than L Q deviation from nominal value!	
Measurement Type Load Correction Data Absolute Measurement	Set Frequencies and Powers         OK       Cancel	

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### Verification

1. Measurement of group delay of the filter without mixer using full two port calibration



#### 2. Measurement of converter (mixer + attenuator + filter )

10 dB

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- Attenuator to avoid that mismatch influences the transmission behavior due to mixer mismatch
- Attenuator has about 40 ps of group delay



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#### **Measurement Result**

Green: Filter without mixer (2-port cal)

Blue:

Converter with calibration with linear mixer



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### **Advantages**

#### Independent of drift of internal LO

• LO has only to be within the IF bandwidth of the ZVA

#### Independent of LO phase noise

- Cancelled out because it acts on both carriers the same way
- Ideal for converters with multiple mixer stages
- Independent of thermal drift of test equipment
  - Only relative measurements
  - Interesting for measurements in thermal chambers

#### No additional external components necessary

• Instead of using an external combiner, the internal coupler can be used as well.



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## Non-Linear VNA measurements

#### The VNA can now do it all

- Harmonics of a signal
- Compression: AM/AM, AM/PM and AM/DM distortions
- Two tone intercept points, 3<sup>rd</sup> and 5<sup>th</sup> order distortion
- S-functions: Generalized non-linear S parameters
- Dynamic Range: Measure Noise Figure and TOI

#### No limitations to the type of DUT

- Measure amplifiers
- Mixers
- Doublers
- Triplers



## Required ZVA Configuration:

<ul> <li>R&amp;S network analyzer with 4 ports</li> </ul>	ZVA or ZVT
<ul> <li>Direct generator receiver access</li> </ul>	ZVA-B16
<ul> <li>Frequency conversion</li> </ul>	ZVA-K4
<ul> <li>Mixer group delay without LO access</li> </ul>	ZVA-K9





#### Conclusions

- A number of different techniques have been employed for making group delay measurements
- The new VNA method derives from established techniques, but makes the measurement task much easier, particularly for frequency-converting devices without LO access





#### **Calibration Mixer**





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